

Evaluating the Drought Code Using *In Situ*  
Drying Timelags of Feathermoss Duff in  
Interior Alaska

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# What is the DC?

- $S = S_0 + P - E_{\text{act}}$
- $E_{\text{act}} = E_{\text{pot}} * S_0/S_{\text{max}}$
- $E_{\text{pot}}$  referenced to an evaporimeter
- $E_{\text{act}}$  causes negative exponential drying
- $E_{\text{act}}$  implies a soil is present
- All we know about the soil is its hydrological properties, water storage capacity,  $S_{\text{max}}$ , and its drying timelag,  $\tau$
- Soil properties cannot be precisely known



# What is the “DC Equivalent Soil”?

- We know its water storage capacity,  $S_{max}$
- Soil parameters are free to vary in fixing  $S_{max}$
- Empirically determine soil attributes from known soils

$$S_{max} = \frac{M_{g,max}}{100\%} \rho \delta$$



# What is the “DC Equivalent Soil”?

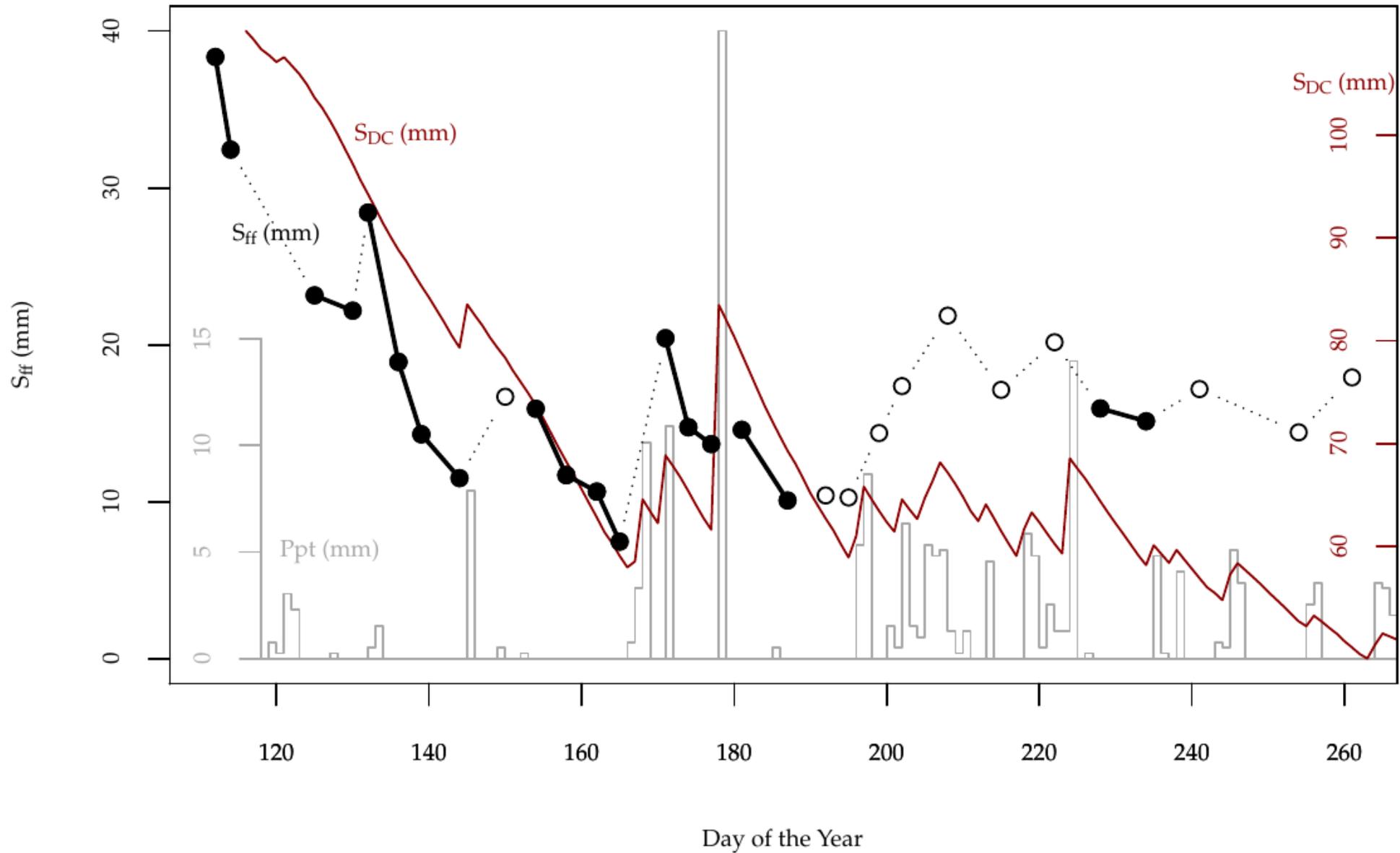
- How can we know the “DC Equivalent Soil”?
- Equate the timelag,  $\tau$ , in a forest floor to that of the DC
- $\tau_{\text{ff}} = \tau_{\text{DC}}$
- Requires a time series of volumetric moisture content measurements



# Wilmore

- Wilmore thesis: “Duff moisture dynamics in black spruce feather moss stands and their relation to the Canadian Forest Fire Danger Rating System”
- 1999 Brenda Wilmore measured MC in a black spruce-feathermoss stand on Fort Wainwright





# Results

- Timelag
- Duff = 28 days
- DC = 60 days
- S<sub>max</sub>
- Duff = 31 mm
- DC = 203 mm



# “DC Equivalent Soil”

- Duff timelag = 28 d and DC timelag = 60 d
- How do we equate timelags to know the properties of the “DC equivalent soil”
- For a negative exponential function:
- Translate between water balances:
  - Duff
  - DC water balance model
  - “DC equivalent soil”

$$\tau = \frac{S_{max}}{E_{pot}} = \frac{S_0}{E_{act}}$$



# Pot. Evap in the Forest

$$\tau_{ff} = \frac{S_{max, ff}}{E_{pot, ff}}$$

$$28 = \frac{31}{E_{pot, ff}}$$

$$E_{pot, ff} = 1.1 \text{ mm}$$

Compare to  $E_{pot}$  at an open evaporimeter

$$E_{pot, open} = 3.3 \text{ mm}$$



# Actual Evap in the Forest

Heijmans et al  
measured 0.3 and 0.9  
for closed and open  
PIMA stands.

$$\tau_{ff} = \frac{S_{0,ff}}{E_{act,ff}}$$

$$28 = \frac{17}{E_{act,ff}}$$

$$E_{act,ff} = 0.60 \text{ mm}$$



# $S_{max}$ of “DC Equivalent” Soil

$$\tau_{DC} = \frac{S_{max, DCeq}}{E_{pot, ff}}$$

$$60 = \frac{S_{max, DCeq}}{1.1}$$

$$S_{max, DCeq} = 66 \text{ mm}$$



# What is the depth of the DC<sub>eq</sub> Soil?

$$S_{max, DCeq} = \frac{M_{g,max}}{100\%} \rho_s \delta$$

$$66 = \frac{29\%}{100\%} 0.62 \delta$$

$$\delta = 374 \text{ mm}$$

\*  $M_{g,max} = 29\%$  and  $\rho_s = 0.62$  because they includes mineral soil



# What is the DC equivalent soil?

- “DC equivalent soil” is 37 cm deep
- 46% mineral soil by depth!
- 95% mineral soil by weight!
- Does not represent “burnable” fuel
- Solely a fire danger rating index



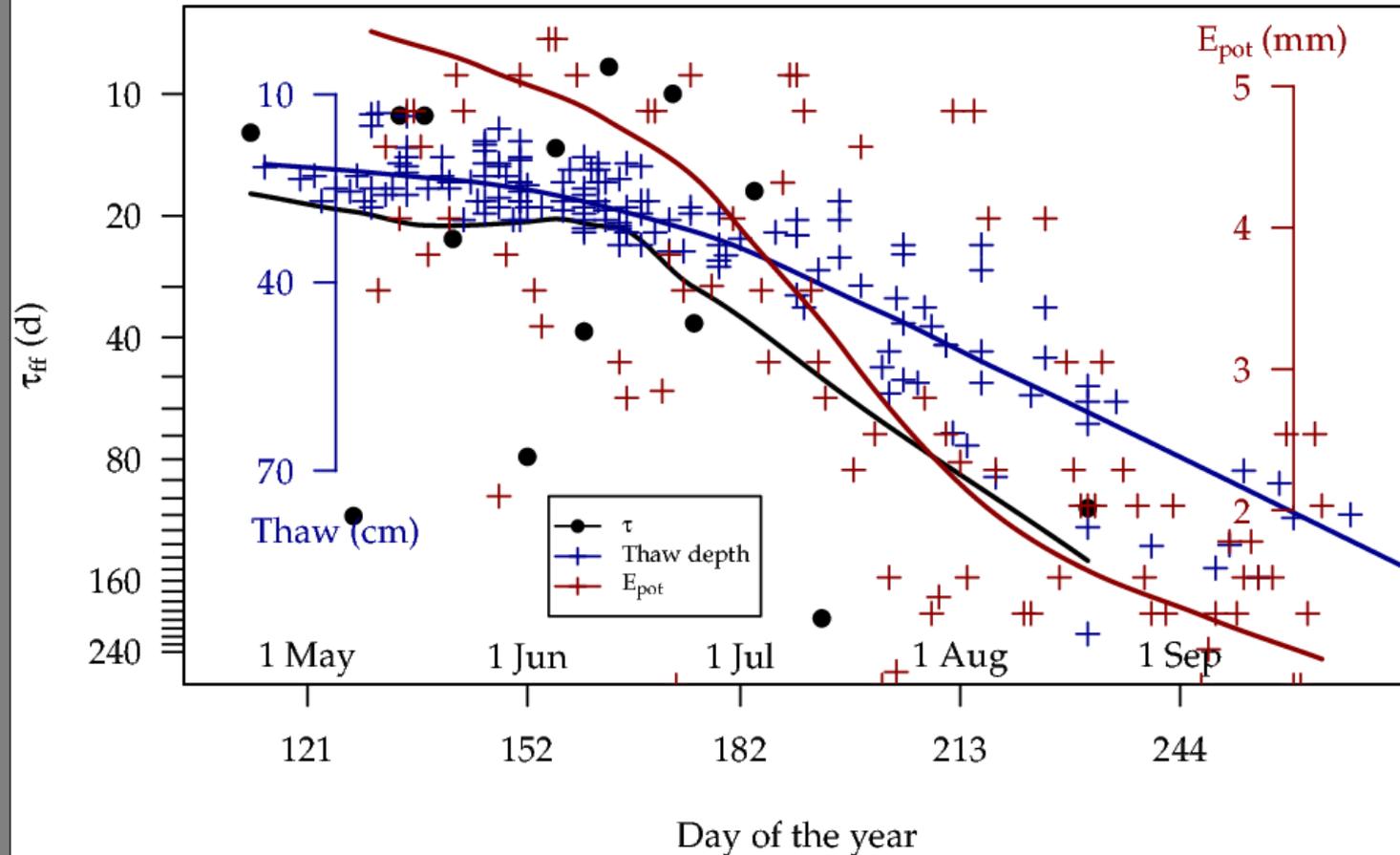
# Permafrost

- DC equivalent soil is 37 cm deep
- Thaw depth reaches 37 cm on 5 July
- $E_{pot}$  peaks in June

$$\tau = \frac{S_{max}}{E_{pot}} = \frac{Low}{High} = Short \tau$$



# Permafrost



$$\tau = \frac{S_{max}}{E_{pot}}$$



# Cross-walk to FWI

Horizon	Thickness	Moisture Code
Live Moss	0-3 cm	FFMC
Dead Moss	3-8	DMC
Upper Duff	8-15	DC
Lower Duff	15-20	
Mineral Soil	20+	

Profile	Thickness	Moisture Code
Live Moss-Mineral Soil	0-37 cm	DC

